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CALCULATION OF COKING CHARGES ON THE BASIS OF  
PETROGRAPHIC CHARACTERISTICS OF COALS

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There is no method available at present in the coking industry for calculating coal charges for producing coke with predetermined physico-mechanical characteristics.

Side by side with this, the coal classification based on the yield of volatile and the thickness of the plastic layer does not reflect their coking characteristics and does not permit to use them more extensively and correctly for coke making. It is well known that the yield of volatiles in most cases does not reflect the true metamorphism of the coals. The difference among them would be more pronounced the more nonuniform is their petrographic composition, the greater is the ash content, and the higher is the state of coal oxidation. Only in coals containing more than 80% vitrinite and but little leiptinite, which are found at the middle stages of metamorphism, there is no difference between the yield of volatiles and the true metamorphism. As far as the thickness of the plastic layer is concerned, the plastometric method is not sufficiently objective, while in application to more metamorphosized coals it is not sensitive. In coals of the SS, and partially of K<sub>2</sub>, types, found in the IV<sub>3</sub>-V<sub>1</sub> stages of metamorphism and containing well caking vitrinite, it is not possible to determine by the plastometric method the thickness of the plastic layer. In these cases the coal is characterized by  $y = 0$  mm.

It has been established that the composition and properties of coals depend on many factors, such as original material, conditions of accumulation, chemical character and water content of the surroundings, degree of metamorphism,

etc. A most complete characteristic of coals can be obtained by supplementing the conventional characteristics with the results of their study by means of new coal petrography methods.

Coals, and particularly Kuznetsk basin coals, vary widely in their petrographic characteristics. Each seam can be considered here as a natural charge. The relation of "fusible" components, of the group of vitrinite and leiptinite, and "infusible" (leaning) of the group of fusinite and the major portion of the components of the semi-vitrinite group, varies in the Kuznetsk basin widely. (The fusibility of the vitrinite and leiptinite groups components varies with the stage of metamorphism of the coal). Thus the content of the leaning components varies in the range of 5 to 65% and of "fusible" ones between 95 and 35%. Depending on the stage of metamorphism, these variations of the proportions have a different effect on caking.

Besides metamorphism, the "fusibility" of the vitrinite group components is affected by their degree of reduction and oxidation.

Before offering a new principle of charge formulation, the petrology laboratory of the Institute of Mineral Fuels of the Academy has investigated during 1952-1954 all major seams of all mines of the Kuznetsk basin. In this work much attention was given to the petrography of coal. As the theoretical basis for the application of the new method served investigations in which were examined basic causes determining different properties of coals. (1)

The stage of metamorphism was determined by the reflectivity. Calculation of the "fusible" components  $\sum FC$  and "lean" ones  $\sum LC$  present in coal was made in accordance with the decisions of the all-Russian conference of coal petrographers. In this connection, as "fusible" components were considered components of the vitrinite group  $V_t$ , of leiptinite  $L$  and  $1/3$  of the components

of the semi-vitrinite group Sv. As leaning components are grouped together fusinite group components F and  $2/3$  of those of the semi-vitrinite group Sv. Here  $\sum FC + \sum LC = 100\%$  of the organic part of the coal. In Table 1 are shown the stages of metamorphism of coals according to I. Annosov.

Table 1. Stages of coal metamorphism.

Approximate kind and group of coal	Metamorphism stage	Indices of subdivisions of metamorphism stages in sub-groups
Brown	zero	$0_1$ $0_2$ $0_3$
Long flame (cannel)	first	$I_1$ $I_2$ $I_3$
Gas coal	second	$II_1$ $II_2$ $II_3$
Bituminous	third	$III_1$ $III_2$ $III_3$
Coking	fourth	$IV_1$ $IV_2$ $IV_3$
Lean coking	fifth	$V_1$ $V_2$ $V_3$
Lean	sixth	$VI_1$ $VI_2$ $VI_3$
Lean highly metamorphosized	seventh	$VII_1$ $VII_2$ $VII_3$
Anthracite	eighth	$VIII_1$ $VIII_2$ $VIII_3$

On the basis of the degree of metamorphism and petrographic composition new characteristics have been established - index of leanness and coking coefficient.

Index of leanness is the relation between the leaning components present in the charge  $\sum LC$  and the amount of leaning components  $\sum LC'$  required for a given charge in order to achieve the optimum relation between fusible and leaning components.

The leaning components both improve and deteriorate coke quality depending on how much of them are added to the coking coal, which is the stage of metamorphism of this coal, and what are the operating conditions. It is evident that one must know the amount of leaning components to be introduced into the charge for the best quality of metallurgical coke.

$\sum LC^1$  is determined by the formula

$$\sum LC^1 = \frac{\sum FC_1}{a_1} + \frac{\sum FC_2}{a_2} + \dots + \frac{\sum FC_n}{a_n}$$

where  $\sum FC_1$   $\sum FC_2$   $\sum FC_n$  is the sum of "fusible" components of the coals of the charge of given stages of metamorphism;  $a_1, a_2, \dots, a_n$  optimum relation between "fusible" and leaning components for corresponding degrees of metamorphism (the optimum relations are determined experimentally). For coals having the stage of metamorphism of  $III_1-III_3$ , for example, for each per cent of leaning components are required 2 per cent of "fusible" components, for  $IV_1-IV_2$  are needed 6%, etc. This is shown in the diagram of Figure 1.

Coking coefficient which characterizes "fusible" components is determined by the formula

$$K = \frac{\sum FC_1 \times K_1 + \sum FC_2 \times K_2 \dots + \sum FC_n \times K_n}{\sum_1^n FC}$$

where  $K_1, K_2 \dots K_n$  are coefficients of coking of the corresponding stages of metamorphism with a given content of the leaning components in the charge. They are graphically presented in the diagram of Figure 2.

Tumbler residue is determined by the index of leanness and coking coefficient on the classification diagram for multicomponent coking charges, Figure 3.

As an example can be given the calculation of the production charge of the Kuznetsk works, Table 2.

Table 2. Production charge of the Kuznetsk metallurgical works from 8/1/'56 to 8/8/'56.

Mine	Components of the coal charge %			Fusinite Content	Σ LC	Σ FC	a	K
	Type	Metamorphism						
Kapitalnaya 1	Zhl	III <sub>1</sub> - III <sub>3</sub>	25	8	2.0	23.0	2.0	5.46
Kapitalnaya 2								
Koksovaya 2	K	IV <sub>1</sub> - IV <sub>2</sub>	10	30	3.0	7.0	6.0	6.42
Stalinskaya	K	IV <sub>1</sub> - IV <sub>2</sub>	12	34	4.1	7.9	6.0	6.42
Vakhrusheva No.3	K <sub>1</sub>	IV <sub>1</sub> - IV <sub>2</sub>	13	17	4.8	8.2	6.0	6.42
Stalinskaya No.3	K <sub>2</sub>	IV <sub>3</sub> - V <sub>1</sub>	13	42	5.6	7.4	16.0	6.0
Zyryanovskaya	PZh-G	II <sub>2</sub> - II <sub>3</sub>	7	8	0.6	6.4	2.5	4.40
Voroshilova	SS	IV <sub>1</sub>	12	51	6.1	5.9	4.4	6.42
Tom Usinskaya No.1,2	KZH2	III <sub>3</sub>	8	43	3.4	4.6	2.5	5.70

$$\sum LC^1 = \frac{23.0}{2.0} + \frac{7.0}{6.0} + \frac{7.9}{6.0} + \frac{8.2}{6.0} + \frac{7.4}{16.0} + \frac{6.4}{2.5} + \frac{5.9}{4.4} + \frac{4.6}{2.5} = 21.6$$

$$K = \frac{23.0 \times 5.46 + 7.0 \times 6.42 + 7.9 \times 6.42 + 8.2 \times 6.42 + 7.4 \times 6.00 + 6.4 \times 4.4 + 5.9 \times 6.42 + 4.6 \times 5.7}{70.4} = 5.83$$

According to the parameters given in the classification diagram, the tumbler residue should be 327 kilograms. The production results gave for the tumbler residue 327 kilograms.

Many calculations made at IGI (2) as well as the calculations of the coke laboratory of the Kuznetsk Metallurgical Works (3) have established that

the difference between the calculated and the production test results in the majority of cases lies between 4 and 5 kilograms. There are reasons to believe that under conditions of a constant method of preparation of the multicomponent charges and a constant coking practice this difference will be reduced.

How well the calculated index of the tumbler residue agrees with the actual one shows the correlation coefficient calculated on the basis of 44 tumbler prognoses as related to experimental coking of different charges containing 7.41-9.08% ash. It happened to be 0.827. The accuracy of determination of the coefficient of correlation can be increased by additional experiments.

In compounding charges the following points should be considered:

(1) better caking can be obtained on coking charges composed of coals close to each other in respect to their degree of metamorphism and (2) the maximum fissuring is produced when there is a considerable difference among the stage of metamorphism of the charge components. On this account, one should not introduce into a charge having a high concentration of gas coals having the metamorphism stage of  $II_1-II_2$  a large proportion of SS coals, the stage of metamorphism of which ranges between  $IV_1$  and  $VI_1$ , or vice versa.

On the basis of many experiments, two types of charges are recommended:

1. from coals having the metamorphism stage of  $II_2$  to  $IV_2$
2. from coals having the metamorphism stage of  $III_1$  to  $V_1$

It has been established that Charge 1 containing an appreciable amount, more than 20%, of coals with metamorphism stage of  $II_2 - II_3$  can take not more than 30% of leaning components; any further increase of the latter sharply affects coke quality. Charge 2 can take 33% of leaning components. It has been also

established that, with the present coking practice, the influence of the leaning components on the quality of coke made of coals having metamorphosis stage of from  $II_3$  to  $V_1$  is about the same. Differences in the behavior of leaning components of coals having different stages of metamorphosis are, apparently, slight and are therefore but little noted during coking.

#### Conclusions:

1. The proposed method can be used for compounding multicomponent coking charges with up to 25% gas coals containing fusain. For a more precise compounding of charges involving spores gas coals, as well as of charges composed of but a few components, additional investigations are in order.

2. Petrographic analysis can be employed for the current control of coals used for coking. It appears more reliable than the other existing methods, particularly for coals made of a mixture of coals from different seams and for coals with an advanced stage of metamorphosis having the plastic layer greater than 7 mm.

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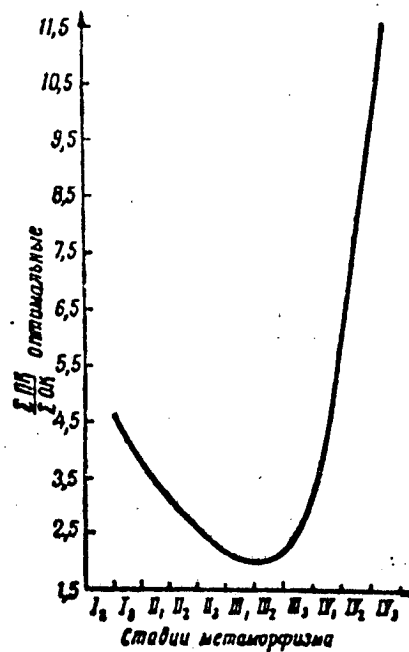


Figure 1. Optimum relation between "fusible" and leaning components of coals having different degree of metamorphism  
 Abscissae: Stages of metamorphism  
 Ordinates: Optimum  $\leq FC / \leq LC$

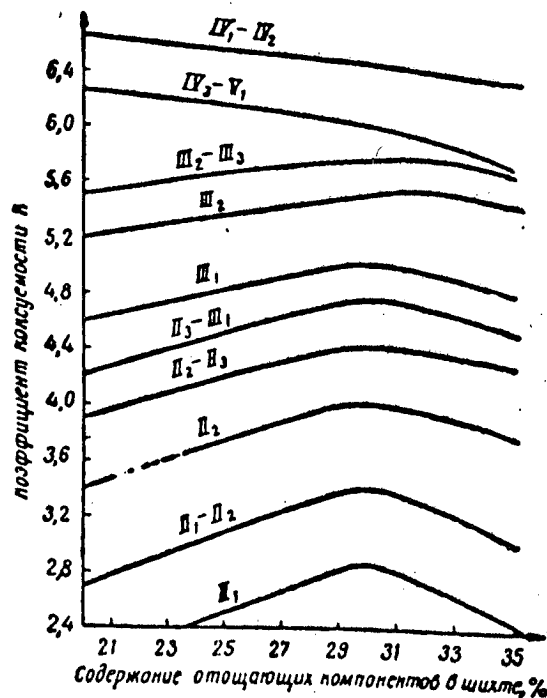


Figure 2. Dependence of the coking coefficient on the stage of metamorphism and the concentration of the leaning components in the charge.

Abscissae: Concentration of leaning components in charge  
 Ordinates: Coking coefficient

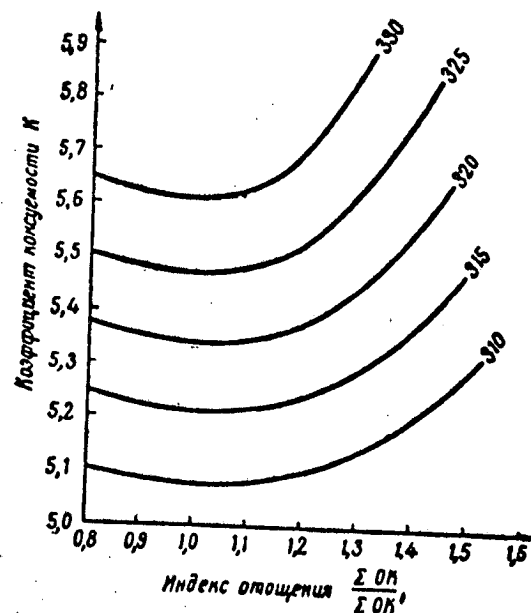


Figure 3. Classification of coking charges for Kuznetsk and Chelyalinsk plants. Curves present identical residues in a standard tumbler.

Abscissae: Index of leaning  $\leq LC / \leq LC'$   
 Ordinates: Coking coefficient K